

# REPORT ON PRELIMINARY SOIL INVESTIGATIONS FOR THE PROPOSED CONSTRUCTION OF TSERC OFFICE BUILDING AT KALYAN NAGAR, S.R. NAGAR, HYDERABAD, TELANGANA.



FOR THE SECRETARY, TELANGANA STATE ELECTRICITY REGULATORY COMMISSION, RED HILLS, HYDERABAD.



### REPORT ON PRELIMINARY SOIL INVESTIGATIONS FOR THE PROPOSED CONSTRUCTION OF TSERC OFFICE BUILDING AT KALYAN NAGAR, S.R. NAGAR, HYDERABAD, TELANGANA.

## 1.0 INTRODUCTION :

1.1 The Secretary, Telangana State Electricity Regulatory Commission, Red Hills, Hyderabad has entrusted the work of conducting preliminary Soil Investigations for the proposed Construction of TSERC Office Building at Kalyan Nagar, S.R. Nagar, Hyderabad, Telangana (Vide Work Order No. A-OA-158, dated 03.09.2022). The aim of this report is to evaluate the nature and depth of the soils and strata at the site, and to determine the safe bearing capacity of the foundations, accordingly. The methods and procedures adopted in the soil investigations are to provide the clients a general idea in the shortest duration possible and are in no way to replace the detailed investigations as Per Standards. Also this report cannot be used as a legal document as the scope of work is very limited in its nature.

## 2.0 **PROJECT DETAILS :**

## 2.1 The Site :

2.1.1 The site for the proposed structure is located at Kalyan Nagar X Roads which is about 13 Km. from MGBS, Hyderabad. The topography of the site area is highly undulated. Site plan with location of boreholes drilled at the site is given in Page No.

## 2.2 STRUCTURE :

2.2.1. As per the clients information the proposed structure is an RCC framed structure comprises of Stilt and Five Upper Floors.



### 2.3 Weather Conditions :

2.3.1 Weather was clear and dry during field investigations, which were carried out in the month of September, 2022.

### 2.4 Seismic Zone :

2.4.1 The proposed project site is situated near Hyderabad, which falls under Seismic Zone II as per IS 1893 (Part I) – 2002.

## 3.0 OBJECT OF INVESTIGATIONS :

- 3.1 For designing the foundation system of the proposed structure, the following data are required :
  - a) Type of foundation system.
  - b) Depth below the ground level at which the foundation system is to be laid.
  - c) Allowable bearing pressure on the foundation at different depths.
- 3.2 To determine above factors, the following information would be required :
  - a) The sub soil profile indicating thickness of the various soil strata, to a depth down to the influence zone below the foundations.
  - b) Engineering properties of the soil strata at various levels.
  - c) Physical characteristics of the soil strata.
  - d) Variation of the strength of the strata with depth.



- 3.3 For evaluating the above parameters, field investigations and laboratory tests on the soil samples collected during the field investigations have been carried out.
- 3.4 The results from these investigations have been analyzed to provide the recommendations for the design of foundations.
- 3.5 These recommendations are valid for the investigated locations only.

## 4.0 SCOPE OF INVESTIGATIONS :

- 4.1 In order to achieve the above objectives, the scope of investigations given by the client includes the following :
  - a) Drilling Four boreholes at four specified locations as shown by the clients upto depths between 12.0M to 15.0M below existing groundlevels with Percussion Drilling Method as Per IS 1892.
  - b) Collection of Disturbed and Undisturbed soil samples in the foundation Pits.
  - c) Conducting calibrated standard penetration tests at regular intervals in the foundation Pits.
  - d) Conducting relevant laboratory tests on soil samples recovered.
  - e) Preparation and submission of a technical report containing the details of the tests carried out, their analysis and recommendations regarding the foundation system to be adopted.



## 5.0 FIELD INVESTIGATIONS :

## 5.1 **Preliminary Details :**

5.1.1 Field investigations was carriedout in the month of September, 2022.

## 5.2 BOREHOLES :

- 5.2.1 The boreholes were drilled at the specified location as shown by the client.
- 5.2.2 The termination depth of the boreholes below Original GL are given in the following table.

Bore Hole No.	Termination Depth from Existing GL (m)	Water Table below the Existing GL (m)
1	15.0	Not met
2	12.0	Not met
3	12.0	Not met
4	13.0	Not met

- 5.2.3 The following operations were undertaken in the borehole.
  - i. Conducting standard penetration tests.
  - ii. Collecting undisturbed samples.
- 5.2.4 Disturbed soil samples recovered from the split spoon sampler were packed in polythene bags and retained for identification purposes.



- 5.2.6 Undisturbed soil samples were recovered by thin walled shell by tubes conforming to IS 2132. These tubes had an area ratio of less than 10%.
- 5.2.7 The diameter of soil samples were 50 mm and its length was 45 cm. However in the refusal strata samples of smaller lengths were collected as further penetration was not practical.
- 5.2.8 The ends of sample tubes were sealed by wax to prevent loss/ ingress of moisture.
- 5.2.9 Standard Penetration tests were conducted as per IS 2131 1981.

#### 6.0 LABORATORY INVESTIGATIONS :

- 6.1 The soil samples brought to the laboratory were tested to evaluate the following properties.
  - a) Type of soil and its gradation
  - b) Consistency limits
  - c) Natural density
  - d) Natural water content
  - e) Shear strength properties
- 6.2 In order to determine the above properties the following tests have been conducted.
  - a) Sieve analysis on the coarse grained soil fraction
  - b) Hydrometer analysis on the fine grained soil fraction
  - c) Liquid and plastic limits
  - d) Natural Density and Water Content tests
  - e) Triaxial Shear tests



### 7.0 **RESULTS OF INVESTIGATIONS :**

- 7.1 The results of field investigations and laboratory tests conducted on the soil samples collected from the borehole have been presented in the form of soil profile tables.
- 7.2 The soil profile tables (Table No 1) as well as the compiled soil profile (Figure 2) gives the details of the strata including their classification and strength properties as ascertained from the tests conducted.
- 7.3 The soil profile tables indicate the following :
  - a) Standard Penetration Test Values (i.e. N- values observed) at various depths.
  - b) Soil description identifying the type of soil.
  - c) In-situ bulk density and Water content.
  - d) Triaxial Shear test results.

#### 8.0 ANALYSIS OF RESULTS :

8.1.1 The compiled subsoil profile as determined from the results of the field and laboratory investigations has been presented in **Table 1**.



i.	Stratum I	: Filled up
ii.	Stratum II	: Clayey Silty Sand with Gravels
iii.	Stratum III	: Highly Weathered Rock with Lime/Clay intrusions
iv.	Stratum IV	: Weathered Rock with Lime/Clay intrusions

v.	Stratum V	:	Soft Disintegrated Rock
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Bore Hole No	(Depth in m : from - to -)								
	Stratum I	Stratum II	Stratum III	Stratum IV	Stratum V				
BH 1	0.0 - 5.0	-	-	5.0 - 7.0	7.0 - 15.0				
BH 2	0.0 - 3.0	3.0 - 4.5		4.5 - 7.0	7.0 - 12.0				
BH 3	0.0 - 4.5	-	-	4.5 - 12.0	-				
BH 4	0.0 - 3.0	-	3.0 - 3.1	3.1 - 13.0	-				

## 9.0 DESIGN CRITERIA :

- 9.1 Design of Foundations :
- 9.1.1 As per the clients information the proposed structure is a RCC framed structure.



- 9.1.2 The design of foundation depends upon the founding strata, loading intensity at the foundation level and configuration at loading points.
- 9.1.3 For the above conditions, Open foundations are recommended for the proposed structure. The footings may be either isolated or combined depending upon the column loads, their spacing and configuration.

#### 9.2 DEPTH OF FOUNDATIONS :

- 9.2.1 Minimum depth of foundations is governed by the following factors :
  - a) Top loose zone.
  - b) Adequate depth of soil above founding level, to ensure mobilization of full safe bearing capacity.
  - c) Adequate depth of soil strata below founding level of requisite strength to mobilize the safe bearing capacity and at the same time restricts the total and differential settlements within the allowable limits.
- 9.2.2 The actual depth of foundation shall be decided by the design engineer.

#### 9.3 ALLOWABLE BEARING PRESSURE :

9.3.1 Typical calculation for allowable bearing pressure is given in **Appendix-1 to 4** may be adopted.



#### **10.0 RECOMMENDATIONS :**

a) Type of Found	lations :	Open
b) Type of Footir	ıg :	Isolated

**c)** Allowable Bearing Pressure : Allowable bearing pressure as given in the following table may be adopted.

10.0

Foundation		Strata	Location	Allowable	Allowable
Depth (m)	Width (m)			Settlement (mm)	Bearing Pressure (tons/m²)
5.00 (Below existing GL)	1.50	Weathered Rock with Lime/ Clay intrusions	BH 1	25	27
4.50 (Below existing GL)	1.50	Weathered Rock with Lime/ Clay intrusions	BH 2	25	<mark>26.5</mark>
4.50 (Below existing GL)	1.50	Weathered Rock with Lime/ Clay intrusions	BH 3	25	<mark>27.5</mark>
4.00 (Below existing GL)	1.50	Weathered Rock with Lime/ Clay intrusions	BH 4	25	26.7

## **11.0 PRECAUTIONS:**

- 11.1 Entire report should be studied before implementing the recommendation
- 11.2 Loose pockets of soil if encountered shall be removed and backfilled with concrete. A leveling course of concrete shall be laid and construction of foundations can be taken up subsequently.



#### 12.0 LIMITATIONS:

- 12.1 The soil investigations have been carried out at locations in the site chosen by the client so as to represent the entire site. The recommendations provided in this report are hence valid only for these test locations. However, if there is any change in sub soil conditions and properties at places between or beyond chosen test locations, Sai Geotechnical Services may be contacted for further advice.
- 12.2 With passage of time, the recommendations may vary due to manmade and natural environmental changes.

#### **13.0 REFERENCES :**

13.1 A list of IS codes referred for providing the recommendations and that which might be required to implement the same has been given in Appendix-3.

for SALGECHECHNICAL SERVICES, HYD STHURI NADH, (IIT Madras), M.IS.T.E Chief Consultant.



**APPENDIX - 1** 

## **CALCULATIONS FOR ALLOWABLE BEARING PRESSURE**

## SHEAR FAILURE CRITERION (Ref. IS: 6403)

### Soil Properties as in the BH 1

Depth of foundation	ns	D	=	500 cm
Width of foundation	n	В	=	150 cm
Length of foundati	on	L	=	150 cm
Angle of shearing re	esistance	φ	=	32°
Cohesion		С	=	0.05 kg/cm <sup>2</sup>
Natural density		γ	=	$1.73 \text{ g/cm}^3$
Submerged density		γb	=	$0.73 \text{ g/cm}^3$
Bearing Capacity Factors	$N_c = 2$	18.07 N	q = 9	$0.75 N_{\gamma} = 8.44, N_{\phi} = 3.25$
Shape Factors		$S_c = 1.3$	30, S	$S_q = 1.20, S_\gamma = 0.80$
Depth factors	$d_c = 2.20$	), $d_q = 1$ .	60, d	$\gamma = 1.60$
Inclination factors	$i_c = i_q = i$	$i_{\gamma} = 1.0$		
Water table factor	W' = 0.5			
Colo Domina Consulta (m				

# Safe Bearing Capacity (under Submerged conditions)

$$q_{s} = 1/3 \left[ 2/3C N_{c} s_{c} d_{c} i_{c} + \gamma_{b} D_{f} (N_{q} - 1)S_{q} d_{q} i_{q} + 0.5 \gamma_{b} B N\gamma S\gamma d\gamma i\gamma W' \right]$$

$$q_{s} = 2.72 \text{ kg/cm}^{2} = 27.2 \text{ t/m}^{2}$$

## **SETTLEMENT CRITERION**

Bearing Pressure for 25 mm settlement

Where	Ν	=	N - value	=	45
	W′	=	water table correction factor	=	0.50
	R <sub>d</sub>	=	depth factor = [1+0.2D/B]≤ 1.2	=	1.20
	D	=	depth of foundation	=	5.00 m
	В	=	width of footing	=	1.50 m

Substituting the values in the above equation we get:

 $q_n = 0.346 \text{ (N-3)} [(B + 0.3)/2B]^2 \text{ W}' \text{ R}_d$ 

$$q_n = 3.14 \text{ kg/cm}^2 = 31.4 \text{ t/m}^2$$

#### Allowable Bearing Pressure

The lower value of the allowable bearing pressure shall be adopted. Therefore, adopt an allowable

bearing pressure of:

q<sub>a</sub> = 2.7 kg/cm<sup>2</sup> i.e. 27.0 tons/m<sup>2</sup>

Note: qa is a NET VALUE, Weight of backfill etc. need not be added to the loading except in case of filling above original Ground Level.



APPENDIX - 2

### **CALCULATIONS FOR ALLOWABLE BEARING PRESSURE**

#### Shear Failure Criterion (Ref. IS: 6403)

## Soil Properties as in the BH 2

Depth of foundation	S	D	=	450 cm
Width of foundation		В	=	150 cm
Length of foundation	1	L	=	150 cm
Angle of shearing res	istance	φ	=	32°
Cohesion		С	=	0.05 kg/cm <sup>2</sup>
Natural density		γ	=	$1.83 \text{ g/cm}^{3}$
Submerged density		γb	=	$0.83 \text{ g/cm}^3$
Bearing Capacity Factors N	$V_{\rm c} = 18.0^{\circ}$	7 N	q = 9	0.75 $N_{\gamma} = 8.44$ , $N_{\phi} = 3.25$
Shape Factors	Sc	= 1.3	0,S	$_{\rm q}$ = 1.20, $S_{\rm \gamma}$ = 0.80
Depth factors c	$l_c = 2.08, d_q$	= 1.5	54, d	$\gamma = 1.54$
Inclination factors i	$i_{c} = i_{q} = i_{\gamma} = 1$	1.0		
Water table factor V	V' = 0.5			
	1 0 1			1

## Safe Bearing Capacity (under Submerged conditions)

$$\begin{array}{l} q_{\rm s} = 1/3 \left[ 2/3 C \ N_{\rm c} \ s_{\rm c} d_{\rm c} i_{\rm c} + \gamma_b \ D_{\rm f} \ (N_{\rm q} - 1) S_{\rm q} d_{\rm q} i_{\rm q} + 0.5 \ \gamma_b \ B \ N\gamma \ S\gamma \ d\gamma \ i\gamma \ W' \right] \\ q_{\rm s} = 2.67 \ kg/cm^2 = 26.7 \ t/m^2 \end{array}$$

## **SETTLEMENT CRITERION**

Bearing Pressure for 25 mm settlement

Where	Ν	=	N - value	=	44
	W′	=	water table correction factor	=	0.50
	R <sub>d</sub>	=	depth factor = [1+0.2D/B]≤ 1.2	=	1.20
	D	=	depth of foundation	=	4.50 m
	В	=	width of footing	=	1.50 m

Substituting the values in the above equation we get:

$$q_n = 0.346 \text{ (N-3)} [(B + 0.3)/2B]^2 \text{ W}' \text{ R}_d$$

$$q_n = 3.06 \text{ kg/cm}^2 = 30.6 \text{ t/m}^2$$

#### Allowable Bearing Pressure

The lower value of the allowable bearing pressure shall be adopted. Therefore, adopt an allowable bearing pressure of:

q<sub>a</sub> = 2.65 kg/cm<sup>2</sup> i.e. 26.5 tons/m<sup>2</sup>

Note: qa is a NET VALUE, Weight of backfill etc. need not be added to the loading except in case of filling above original Ground Level.



#### APPENDIX - 3

# **CALCULATIONS FOR ALLOWABLE BEARING PRESSURE**

## Shear Failure Criterion (Ref. IS: 6403)

### Soil Properties as in the BH 3

Depth of foundation	ons	D	=	450 cm
Width of foundation	n	B	=	150 cm
Length of foundati	on	L	=	<mark>150 c</mark> m
Angle of shearing r	esistance	φ	=	32°
Cohesion		С	=	0.05 kg/cm <sup>2</sup>
Natural density		γ	=	1.87 g/cm <sup>3</sup>
Submerged density		γb	=	0.87 g/cm <sup>3</sup>
Bearing Capacity Factors	$N_c = 18.07$	7 N	<sub>q</sub> = 9	$N_{\gamma} = 8.44, N_{\phi} = 3.25$
Shape Factors	$S_c =$	= 1.3	0, S	$_{\rm q}$ = 1.20, $S_{\gamma}$ = 0.80
Depth factors	$d_c = 2.08, d_q$	= 1.5	54, d	$\gamma = 1.54$
Inclination factors	$i_c = i_q = i_\gamma = 1$	.0		
Water table factor	W' = 0.5			
	1 0 1			1

## Safe Bearing Capacity (under Submerged conditions)

$$\begin{array}{l} q_{\rm s} = 1/3 \left[ 2/3 C \ N_{\rm c} \ s_{\rm c} d_{\rm c} i_{\rm c} + \gamma_{\rm b} \ D_{\rm f} \ (N_{\rm q} - 1) S_{\rm q} d_{\rm q} i_{\rm q} + 0.5 \ \gamma_{\rm b} \ B \ N\gamma \ S\gamma \ d\gamma \ i\gamma \ W' \right] \\ q_{\rm s} = 2.77 \ kg/cm^2 = 27.7 \ t/m^2 \end{array}$$

## **SETTLEMENT CRITERION**

Bearing Pressure for 25 mm settlement

Where	Ν	=	N - value	=	45
	W′	=	water table correction factor	=	0.50
	R <sub>d</sub>	=	depth factor = [1+0.2D/B]≤ 1.2	=	1.20
	D	=	depth of foundation	=	4.50 m
	В	=	width of footing	=	1.50 m

Substituting the values in the above equation we get:

$$q_n = 0.346 (N-3) [(B + 0.3)/2B]^2 W' R_d$$

$$q_n = 3.14 \text{ kg/cm}^2 = 31.4 \text{ t/m}^2$$

#### Allowable Bearing Pressure

The lower value of the allowable bearing pressure shall be adopted. Therefore, adopt an allowable bearing pressure of:

q<sub>a</sub> = 2.75 kg/cm<sup>2</sup> i.e. 27.5 tons/m<sup>2</sup>

Note: qa is a NET VALUE, Weight of backfill etc. need not be added to the loading except in case of filling above original Ground Level.



**APPENDIX - 4** 

#### CALCULATIONS FOR ALLOWABLE BEARING PRESSURE

#### Shear Failure Criterion (Ref. IS: 6403)

Soil Properties as in the B	H 4						
Depth of foundation	ons	D	=	400 cr	n		
Width of foundation	n	B	=	150 cr	n		
Length of foundati	on	L	=	150 cr	n		
Angle of shearing r	esistance	φ	=	32°			
Cohesion		С	=	0.04 k	kg/cm <sup>2</sup>		
Natural density		γ	=	1.64 g	g/cm <sup>3</sup>		
Submerged density		γb	=	0.64 g	g/cm <sup>3</sup>		
Bearing Capacity Factors	$N_c = 24.22$	2 N	q = 1	.3.95 N	Ν <sub>γ</sub> = 16.51,	N <sub>0</sub> = 3.25	
Shape Factors	S <sub>c</sub> =	= 1.3	0,S	<sub>q</sub> = 1.20	$0, S_{\gamma} = 0.80$		
Depth factors	$d_c = 1.96, d_q =$	= 1.4	48, d	γ = 1.48	3		
Inclination factors	$i_c = i_q = i_\gamma = 1$	.0					
Water table factor	W' = 0.5						
Safe Bearing Capacity (u	nder Submer	ged	con	ditions	<u>5)</u>		
$q_s = 1/3 [2/3C N]$	$_{c} s_{c} d_{c} i_{c}$ + $\gamma_{b} D_{f}$	(Nq	- 1)5	S <sub>q</sub> d <sub>q</sub> i <sub>q</sub> +	+ 0.5 γ <sub>b</sub> B N <sup>-</sup>	γ Sγ dγ iγ W	]
$a = 2.67 \ln a / cm^2$	$-267 \pm 10^{2}$						

 $q_s = 2.67 \text{ kg/cm}^2 = 26.7 \text{ t/m}^2$ 

## SETTLEMENT CRITERION

Bearing Pressure for 25 mm settlement

Where	Ν	=	N - value	=	44
	W′	=	water table correction factor	=	0.50
	R <sub>d</sub>	=	depth factor = [1+0.2D/B]≤ 1.2	=	1.20
	D	=	depth of foundation	=	4.00 m
	В	=	width of footing	=	1.50 m

Substituting the values in the above equation we get:

$$q_n = 0.346 (N-3) [(B + 0.3)/2B]^2 W' R_d$$

$$q_n = 3.06 \text{ kg/cm}^2 = 30.6 \text{ t/m}^2$$

#### Allowable Bearing Pressure

The lower value of the allowable bearing pressure shall be adopted. Therefore, adopt an allowable bearing pressure of:

 $q_a = 2.67 \text{ kg/cm}^2 \text{ i.e. } 26.7 \text{ tons/m}^2$ 

Note: qa is a NET VALUE, Weight of backfill etc. need not be added to the loading except in case of filling above original Ground Level.



### **APPENDIX - 5**

# LIST OF IS CODES

#### LABORATORY TESTS

1.	IS 2720 (Part 1) - 1983	:	Preparation of soil samples
2.	IS 2720 (Part 2) - 1973	:	Determination of water content
3.	IS 2720 (Part 4) - 1985	:	Grain Size Analysis
4.	IS 2720 (Part 5) - 1985	:	Atterberg Limits
5.	IS 2720 (Part 11) - 1973	:	Determination of shear Strength parameters using triaxial shear apparatus.

## FIELD INVESTIGATIONS

1.	IS 1498 :	1970	:	Classification and Identification of soils for general engineering purposes.
2.	IS 1892 :	1979	:	Code of practice for sub surface investigations for foundations.
3.	IS 2131 :	1981	:	Method of standard penetration test for soils.
4.	IS 2132 :	1986	:	Code of practice for thin walled tube sampling of soil.





DEGEND: BH : BOREHOLE

SITE: TSERC-KALYAN NAGAR



FIGURE-2														
					COMB	INED S	OIL PI	ROFILE						
	BH 1			BH 2				BH 3				BH 4		
Depth	(m)	N-value	Depth (	m)	N-Value	e	Depth (1	n)	N-Value	, ,	Depth (1	m)	N-Value	
0.25			0.25				0.25				0.25			
0.5			0.5				0.5				0.5			
1.0			1.0				1.0				1.0			
1.5		9	1.5		8		1.5		10		1.5		10	
2.0			2.0				2.0				2.0			
2.5			2.5				2.5				2.5			
3.0			3.0				3.0				3.0			
3.5		10	3.5		14		3.5		11		3.10 3.5		30	
4.0			4.0				4.0				4.0			
4.50		11	4.50				4.50				4.50		44	
5.0			5.0		44		5.0		45		5.0			
5.5		45	5.5				5.5				5.5			
6.0			6.0		45		6.0		46		6.0		45	
6.5			6.5				6.5				6.5			
0.5			7.0				0.5				0.5			
7.0			7.0	,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,			7.0				7.0			
7.5		>75	7.5		>75		7.5		47		7.5		46	
8.0			8.0				8.0				8.0			
8.5			8.5				8.5				8.5			
9.0		>75	9.0		>75		9.0		48		9.0		47	
9.5			9.5				9.5				9.5			
10.0			10.0				10.0				10.0			
10.5		>75	10.5		>75		10.5		49		10.5		48	
11.0			11.0				11.0				11.0			
11.5			11.5				11.5				11.5			
12.0		>75	12.0		>75		12.0		49		12.0		49	
12.5											12.5			
13.0											13.0			
13.5		>75												
14.0														
14.5														
15.0		>75												
			LEG	END:										
					Fille	d up								
					Wea	thered	Roc	k with I	.ime/	Clay i	intrus	ions		
					Soft	Disint	egrat	ed Rocl	۱ ۲					
					High	ly We	ather	ed Rocl	k with	Lime	e/ Cla	y intrus	ions	
			44		Obse	erved N	N - V:	alue Fo	rty Fo	ur ble	ows fo	r 30cm	penet	ratio
						ſ	C	)	v - 5					
							<b>Ç</b>							

SAI GEOTECHNICAL SERVICES

(SOIL INVESTIGATIONS) Neredmet, Secunderabad. Mobile : 9948843777

Property /Bore	Soil	Depth (m)	Specific Gravity	Water Content	Natural Density	Grain	Size Distr	ibution	At	terberg I (%)	limits	Shear Par	ameters
Hole No.		()		(%)	(g/cc)	Gravel > 4.75mm	Sand 4.75 – 0.075mm	Silt+Clay < 0.075mm	Liquid Limit	Plastic Limit	Plasticity Index	Cohesion kg/sq cm	Φ degrees
BH 1	Filling	1.5	2.57	1.4	1.42	12	25	63	-	NP	NP	0.31	20
BH 1	Filling	3.0	2.61	2.1	1.43	14	31	55	_	NP	NP	0.36	21
BH 1	Filling	4.5	2.61	2.8	1.44	15	32	53	-	NP	NP	0.35	22
BH 1	W/Rock with Lime/Clay	5.5	2.70	3.4	1.73	-	-	-	-	NP	NP	0.05	32
BH 1	W/Rock with Lime/Clay	6.5	2.71	4.1	1.80	-	-	-	-	NP	NP	0.04	32
BH 1	SDR	8.0	2.75	5.3	2.04	-	-	-	-	NP	NP	0.03	34
BH 1	SDR	9.5	2.76	6.4	2.06	-	-	-	_	NP	NP	0.02	34
BH 1	SDR	11.0	2.77	7.2	2.08	-	-	-	-	NP	NP	0.01	34
BH 1	SDR	12.5	2.77	8.4	2.08	-	-	-	-	NP	NP	JP 0.01	
BH 1	SDR	14.0	2.77	8.5	2.09	-	-	-	-	NP	NP	0.00	35

TABLE-1 SUMMARY OF SOIL PROPERTIES



## TABLE-1A SUMMARY OF SOIL PROPERTIES

Property	Soil	Depth	Specific	Water	er Natural Grain Size Distribution Atterberg Limit							Shear Par	ameters
/Bore Hole No.		(m)	Gravity	(%)	(g/cc)	Gravel > 4.75mm	(%) Sand 4.75 – 0.075mm	Silt+Clay < 0.075mm	Liquid Limit	(%) Plastic Limit	Plasticity Index	Cohesion kg/sq cm	Φ degrees
BH 2	Filling	1.50	2.61	1.8	1.40	11	30	59	-	NP	NP	0.38	22
BH 2	CL	3.00	2.61	2.6	1.61	12	31	57	35	24	11	0.33	26
BH 2	W/Rock with Lime/Clay	4.50	2.70	3.2	1.83	-	-	-	-	NP	NP	0.05	32
BH 2	W/Rock with Lime/Clay	6.00	2.71	4.3	1.85	-	-	-	-	NP	NP	0.05	33
BH 2	SDR	7.50	2.74	5.2	2.01	-	-	-	-	NP	NP	0.03	34
BH 2	SDR	9.00	2.75	6.4	2.03	-	-	-	-	NP	NP	0.02	34
BH 2	SDR	10.5	2.76	7.2	2.05	-	-	-	-	NP	NP	0.01	34
BH 2	SDR	12.0	2.77	8.4	2.07	-	-	-	-	NP	NP	0	35



Property /Bore	PropertySoilDepthSpecificWaterNaturalGrain Size DistributionAtterber/Bore(m)GravityContentDensity(%)(%)								terberg L	imits	Shear Par	ameters	
Hole No.		(11)	Glavity	(%)	(g/cc)	Gravel > 4.75mm	(76) Sand 4.75 – 0.075mm	Silt+Clay < 0.075mm	Liquid Limit	Plastic Limit	Plasticity Index	Cohesion kg/sq cm	Φ degrees
BH 3	Filling	1.50	2.70	1.3	1.49	-	-	-	-	NP	NP	0.05	28
BH 3	Filling	3.00	2.61	2.4	1.58	12	30	58	-	NP	NP	0.35	22
BH 3	W/Rock with Lime/Clay	4.50	2.70	3.4	1.87	-	-	-	-	NP	NP	0.05	32
BH 3	W/Rock with Lime/Clay	6.00	2.71	4.2	1.88	-	-	-	-	NP	NP	0.05	32
BH 3	W/Rock with Lime/Clay	7.50	2.71	5.3	1.90	-	-	-	-	NP	NP	0.04	33
BH 3	W/Rock with Lime/Clay	9.00	2.71	6.4	1.91	-	-	-	-	NP	NP	0.04	33
BH 3	W/Rock with Lime/Clay	10.5	2.72	7.2	1.92	-	-	-	-	NP	NP	0.04	33
BH 3	W/Rock with Lime/Clay	12.0	2.72	8.4	1.93	-	-	-	-	NP	NP	0.04	33

TABLE-1B SUMMARY OF SOIL PROPERTIES



Property	Soil	Depth	Specific	Water	Natural	Grain	Size Distri	ibution	At	terberg L	limits	Shear Par	ameters
/Bore		(m)	Gravity	Content	Density		(%)			(%)			
Hole				(%)	(g/cc)	Gravel	Sand	Silt+Clay	Liquid	Plastic	Plasticity	Cohesion	Φ
No.						>	4.75 –	<	Limit	Limit	Index	kg/sq	degrees
						4.75mm	0.075mm	0.075mm				cm	
BH 4	Filling	1.50	2.65	1.7	147	-	-	-	-	NP	NP	0.10	28
BH 4	H.W.R. with Lime/Clay	3.00	2.70	2.6	1.74	-	-	-	-	NP	NP	0.05	31
BH 4	W/Rock with Lime/Clay	4.50	2.71	3.4	1.64	-	-	-	-	NP	NP	0.05	32
BH 4	W/Rock with Lime/Clay	6.00	2.71	4.2	1.85	-	-	-	-	NP	NP	0.05	32
BH 4	W/Rock with Lime/Clay	7.50	2.72	5.6	1.87	-	-	-	-	NP	NP	0.04	33
BH 4	W/Rock with Lime/Clay	9.00	2.72	6.4	1.89	-	-	-	-	NP	NP	0.04	33
BH 4	W/Rock with Lime/Clay	10.5	2.72	7.1	1.92	-	-	-	-	NP	NP	0.04	33
BH 4	W/Rock with Lime/Clay	12.0	2.72	8.3	1.93	-	_	_	-	NP	NP	0.04	33

TABLE-1C SUMMARY OF SOIL PROPERTIES



							FIGU	RE-3									
			ETEL D	BOREL			DATA SH	IEET -	PROF		HEET NO (1	•					
			11000	DORE E		BORE	HOLE LO	CATIO	N: BH	1							
6.L. (m)	less (m)	ption of d person	rep.	ampling	ample .L.		SP	PT Deta	uils		Core Recovery Data	overy	(m) a	*	rill / in	rilling	S
Depth below (	Strata thick	Visual Descri strata by fiel	Symbolic	Nature of s	Depth of s below G	Depth (m)	0 - 15 cm S	of Bloo	30 - 45 cr	Corrected N Value	Total length of cores (m)	% Core rec	RQD Value	RQD,	Rate of d 30cm/rr	Colour of d water	Remark
0.00			000	•													
		Filled up	000	SPT	1.5	1.5	1	3	6	9					11		
2.00	2.00		000													Brown	
			000	•													
		Filled up	ତ ତ ତ	DS	1.0	1.0									Avg	-	
3.00	1.00													-	10	Brown	
		Filled up		EPT	3.0	3.0	1		7	10					A.v.a	Bnown	
5.00	1 55	T med up		SPT	4.5	4.5	1		7	11					10	Brown	
5.00	1.55		# # #		4.5	4.5	-	-							10		
		Weathered Rock with Lime/ Clay	###	SPT	5.5	5.5	18	21	24	45		0%		Nil	Avg		
7.00	2.00	intrusions	# # #	•											41	Yellow	
			<u> </u>														
		Soft Disintegrated Rock	$\times \times \times$	SPT	7.0	7.0	60/8 <i>c</i> m	-	-	Refusal		0%		Nil	Avg	Yellow	
9.00	2.00		$\times \times \times$												52		
			$\times \times \times$														
		Soft Disintegrated Rock	$\times \times \times$	SPT	8.5	8.5	62/5cm	-	-	Refusal		0%		nil	Avg	Yellow	
10.50	1.50		$\times \times \times$	SPT	10.0	10.0	65/4cm	-	-	Refusal					54		
			$\times \times \times$														
		Rock	$\times \times \times$	SPT	11.5	11.5	68/3cm	-	-	Refusal		0%		Nil	Avg	Yellow	
12.00	1.50		$\times \times \times$												56		
			$\times \times \times$														
		Soft Disintegrated Rock	$\times \times \times$													Yellow	
13.50	1.50		$\times \times \times$	SPT	13.0	13.0	65/4cm	-	-	Refusal					54		
			$\times \times \times$														
		Soft Disintegrated Rock	$\times \times \times$	SPT	15.0	15.0	68/3cm	-	-	Refusal		0%		Nil	Avg	Yellow	
15.00	1.50		$\times \times \times$												56		



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	FIGURE-3																
			ETELD	BODE L			DATA CL	ICCT	PDOF		FET NO. (2						
			FIELD	BORE L	UG CHAR	BODE				ORMA SI	HEET NO. (2	.)					
L. (m)	ss (m)	ion of person	ġ	pling			SP	PT Deta	uls		Core Recovery	/ery	(m)		<u> </u>	lling	
Depth below G.	Strata thickne	Visual Descript strata by field	Symbolic re	Nature of san	Depth of sar below G.L	Depth (m)	- 15 cm •Z	of Blow 5 08 - 2	0 - 45 cr	Corrected N Value	Total length of cores (m)	% Core reco	RQD Value	RQD, %	Rate of dri 30cm/mir	Colour of dri water	Remarks
0.00			ල ල ල				0	1	e		•						
		Filled up	<u>e e e</u>	SPT	1.5	1.5	1	2	6	8					11		
3.00	3.00		<u>e e e</u>													Brown	
		Clayey Silty Sand	~ ~ ~					_							-		
4.50	1.50	with Gravels	~ ~ ~	SPI	3.0	3.0	1	5	9	14					Avg 15	Brown	
	1.00	Weathered Rock with Lime/ Clay	# # #	•													
			###	SPT	4.5	4.5	16	20	24	44		0%		Nil	Avg	own/ Whi	te
6.00	1.50	intrusions	# # #	•											43		
		Weathand Back	###														
		with Lime/ Clay	###	SPT	6.0	6.0	18	21	24	45		0%		Nil	Avg	own/ Whi	te
7.00	1.00	intrusions	###	•											44		
			ххх														
		Soft Disintegrated	$\times \times \times$	SPT	7.5	7.5	62/6cm	-	-	Refusal		0%		Nil	Avg	Yellow	
9.00	2.00	ROCK	$\times \times \times$												52		
			~ ~ ~														
		Soft Disintegrated Rock	$\times \times \times$	SPT	9.0	9.0	63/4cm	-	-	Refusal	-	0%		nil	Avg	Yellow	
10.50	1.50		$\times \times \times$	SPT	10.5	10.5	65/3cm	-	-	Refusal					54		
		Rock	ххх	SPT	12.0	12.0	70/2cm	-	-	Refusal	-	0%		nil	Avg	Yellow	
12.00	1.50		$\times \times \times$		ļ										56		



							FIGU	RE-3									
			ETELD	BODEL			DATA SI	IEET -	PROF		HEET NO (3	1)					
			1100	DORE		BORE	HOLE LO	CATIO	N: BH 3	3		,					
6.L. (m)	ness (m)	ption of d person	.dar	ampling	ample .L.		SI	PT Deta	uls		Core Recovery Data	covery	e (m)	~	hill /	Irilling .	s
Depth below	Strata thick	Visual Descr strata by fie	Symbolic	Nature of s	Depth of s below G	Depth (m)	0 - 15 cm	of Blow 15 - 30 ct	30 - 45 cr	Corrected N Value	Total length of cores (m)	% Core rei	RQD Valu	KQD,	Rate of a 30cm/r	Colour of c watei	Reman
0.00			666														
		Filled up	@ @ @	DS	1.0	1.0									6		
1.00	1.00		<u> </u>													Brown	
		E.H. dam		CDT	1 5	1 5		2	-	10							
2 00	1 00	Filled up		SPI	1.5	1.5	1	3		10						Brown/ White	
2.00	1.00		000														
		Filled up	000	DS	2.0	2.0									Ava	own/ Whi	te
3.00	1.00		000												8		
			000														
		Filled up	000	SPT	3.0	3.0	1	4	7	11					Avg	Brown	
4.50	1.50		@ @ @												9		
		Weathered Rock	# # #														
		with Lime/ Clay	###	SPT	4.5	4.5	18	21	24	45		0%		Nil	Avg	own/ Whi	te
6.00	1.50	intrusions	# # #	•											44		
		Weathered Rock	# # #														
		with Lime/ Clay	###	SPT	6.0	6.0	17	21	25	46		0%		nil	Avg	own/ Whi	te
8.00	2.00	intrusions	# # #	SPT	7.5	7.5	19	22	25	47					45		
		Weathered Pock	# # #														
		with Lime/ Clay	# # #	SPT	9.0	9.0	18	22	26	48		0%		Nil	Avg	own/ Whi	te
9.50	1.50	intrusions	# # #	•											46		
		Westhand Back	# # #														
		with Lime/ Clay	# # #	SPT	10.5	10.5	20	23	26	49		0%		Nil	Avg	own/ Whi	te
11.00	1.50	intrusions	###	•											47		
			$\mathbf{x} \mathbf{x} \mathbf{x}$														
		weathered Rock with Lime/ Clav	XXX	SPT	12.0	12.0	21	22	27	49		0%		nil	A1/0	Vellow	
12.00	1 00	with Lime/Clay ) intrusions			12.0	12.0	-1		/			0 /8				, enow	
12.00	1.00							1							55		



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							FIGU	RE-3									
FIELD BORE LOG CHART AND DATA SHEET - PROFORMA SHEET NO. (4)																	
BORE HOLE LOCATION: BH 4																	
9.L. (m)	Strata thickness (m) Visual Description of strata by field person	rep.	ampling	ample .L.	SPT Details					Core Recovery Data	overy	e (m)	*	<u>الا</u> ال	rilling	8	
Depth below		Visual Descri strata by fiel	Symbolic	Nature of s	Depth of s below G	Depth (m)	0 - 15 cm י₀N	of Blow 5 12 - 30	30 - 45 cr	Corrected N Value	Total length of cores (m)	% Core rec	RQD Valu	RQD,	Rate of d 30cm/n	Colour of c water	Remar
0.00			~~~														1
		Filled up	@ @ @	DS	1.0	1.0									9	1	
1.00	1.00		@ @ @	•												Brown	
			@ @ @	-													1
		Filled up		SPT	1.5	1.5	1	3	7	10					Avg		
3.00	2.00		# # #												10	Brown	
		Highly Weathered	++ ++ ++								-						
		Clay intrusions		SPT	3.0	3.0	9	13	17	30	_	0%		Nil	Avg	own/ White	
3.10	0.10		# # #												32	ļ	
		Weathered Rock	# # #								-						1
		with Lime/ Clay	###	SPT	4.5	4.5	16	20	24	44		0%		Nil	Avg	own/ White	
5.00	1.90	intrusions	# # #	•											43		1
		Weathered Rock	# # #														1
		with Lime/ Clay	###	SPT	6.0	6.0	18	21	24	45		0%		Nil	Avg	own/ Whi <sup>.</sup>	te
7.00	0 2.00	intrusions	# # #	•											44		1
		Weathered Rock	# # #								_	0%		nil			Ī
		with Lime/ Clay	# # #	SPT	7.5	7.5	17	21	25	46					Avg	own/ White	
8.50	1.50	intrusions	# # #												45		ł
		Weathered Bock	# # #														i i
		with Lime/ Clay	# # #	SPT	9.0	9.0	19	22	25	47		0%		nil	Avg	own/ White	
10.00	1.50	intrusions	# # #												46		ł
			# # #	:													i
		Weathered Rock	# # #	60 <b>T</b>	10 5	10 5			0F	40		<b>0</b> %			<b>.</b>		
		intrusions		SPI	10.5	10.5	20	23	25	48		0%			Avg	own/ whi	re
11.50	1.50		# # #												47	ļļ	
		Weathered Rock	$  \times \times \times  $	. ×	13.0						-	0%					I
		with Lime/ Clay intrusions	$\times \times \times$	SPT		13.0	21	23	26	49				nil	Avg	Yellow	i
13.00	1.50		$\times \times \times$												52		1



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